



Robust ABF for Large, Passive **Broadband Sonar Arrays**

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Introduction: Themes



require particular attention to computing efficiency ABF for large arrays (100 < N < 10000 elements)

Element space DMR > O(ND²)

"Ideal" reduced complexity adaptive beamformer:

- Adaptation space dimension, N_a, close to required adaptive degrees of freedom D
- Consistent with spatial sampling theory
 - Steering direction invariant
- "Robust robustness"

Broadband beamforming:

- computing efficiency inherent at low frequency
- can trade high SNR signal suppression for spatial resolution



LOPS AO Array Wet Subsystem(AWS)



Frunk Terminus Segment (TTS) NSWC PEV

Observatory Trunk Segment (OTS)

Horizontal Array Segment (HAS) 1664

sensors

Off-board
Array Element
Location
Segment
(OAELS)

Non-Development Item (NDI)
Legacy Sensor



Complexity (C) in Dominant Mode Rejection (DMR) Adaptive Beamforming (ABF)

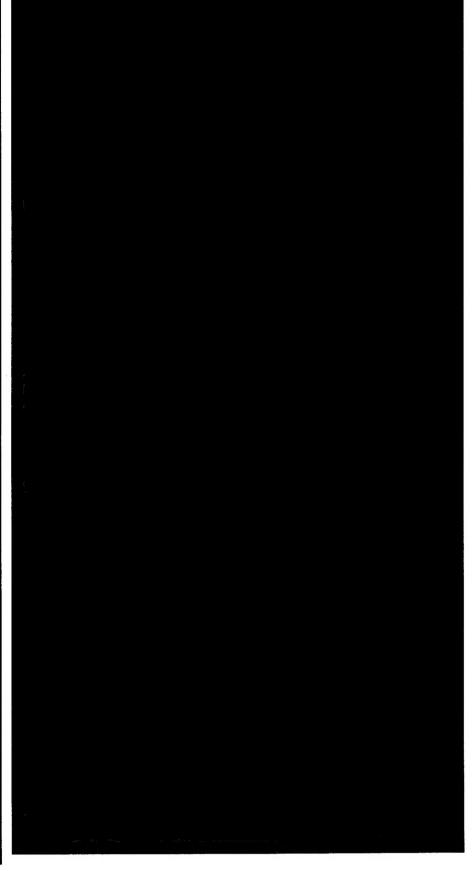


- N = number of sensors
- S = number of steering directions
- N_a = number of adaptively filtered channels
- D = number of adaptive degrees of freedom



Candidate ASAP Methods for Large BB Arrays







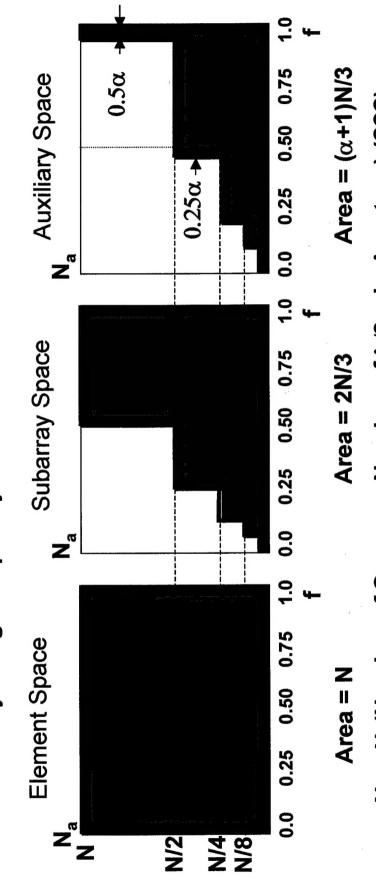
Adaptive Degrees of Freedom: Frequency Dependence



= number of sensors \(\lambda/2\) spaced sensors in linear array

N₂ = number of adaptive channels

= frequency normalized by the $\lambda/2$ spacing design frequency f=1 is array design frequency



 $N_a = N_a(Number of Sources, Number of <math>\lambda/2$ -s in Aperture) (???)



Measures of Performance



- Qualitative: Bearing-Time-Recording (BTR) side-by-side beauty contest
- Quantitative: Array Gain (AG)

 $\mathbf{w}(\theta_{ ang}) = \mathbf{beam}$ forming filter vector for beam steered at $\theta_{ ang}$

 $\mathbf{P}_{\text{true}}(\theta_{\text{targ}}) = \text{Cross-Channel Spectral Density Matrix (CSDM)}$ Trace($\mathbf{P}_{true}(\theta_{targ})$) = N $= \mathbf{d}(\theta_{\text{targ}})\mathbf{d}(\theta_{\text{targ}})^{\text{H}},$

 $Trace(\mathbf{Q}_{true}(\theta_{targ})) = N$ $\mathbf{Q}_{\text{true}}(\text{all}\theta \neq \theta_{\text{targ}}) = \sum_{\mathbf{q}} \alpha_{\mathbf{m}} \mathbf{d}(\theta_{\mathbf{m}}) \mathbf{d}(\theta_{\mathbf{m}})^{\mathrm{H}} + \alpha_{\mathbf{0}} \mathbf{I}_{\mathbf{N}}$,

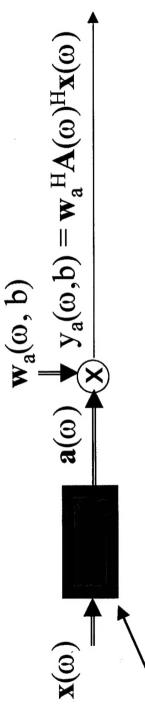
AG MOP Usage

- AG is given as a function of θ_{targ} for static source examples
- clairvoyant designated target tracker for AG is given along the bearing track of a dynamic source examples





ABF with Subarray Preprocessing 🚄



Steering invariant subarray grouping:

$$\mathbf{v}_{a}(\omega, b) = \mathbf{A}(\omega)^{H}\mathbf{v}(\omega, b)$$

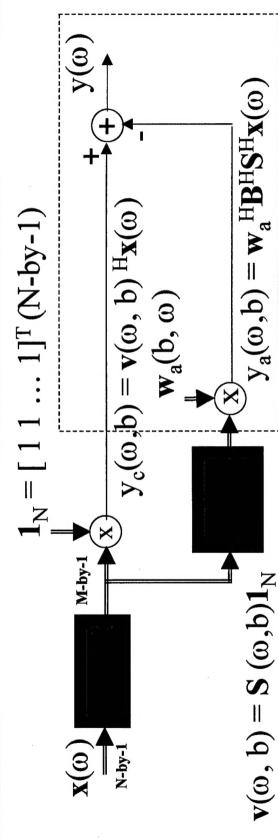
Suppress @ and b notation:

$$\mathbf{W}_{a} = \frac{\mathbf{I}}{\mathbf{V}_{a} \mathbf{R}^{-1} \mathbf{V}_{a}} \mathbf{R}^{-1} \mathbf{V}_{a}$$



Blocking Distortionless Response (DR) GSC with Presteering and Signal





Suppress @ and b notation:

Unconstrained "Weiner Filter"

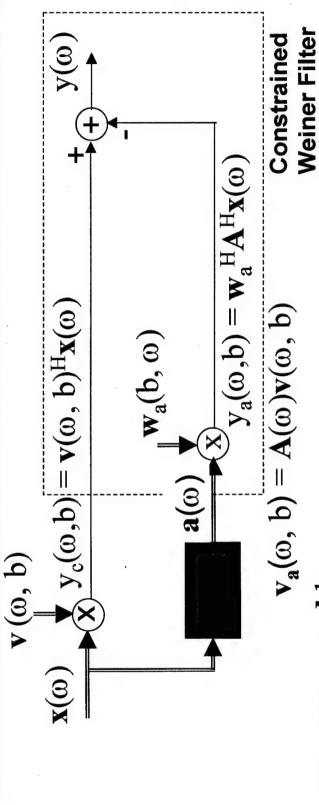
$$\mathbf{B}^{H}\mathbf{1}_{N} = \mathbf{0}_{M} = [0 \ 0 \ \dots \ 0]^{T} (M-by-1)$$

$$\mathbf{w}_{a} = [\mathbf{B}^{H}\mathbf{S}^{H}\mathbf{R}_{xx}\mathbf{S}\mathbf{B}]^{-1}\mathbf{B}^{H}\mathbf{S}^{H}\mathbf{R}_{xx}\mathbf{v}$$



Steering Invariant DR Sidelobe Cancellation (SISC) Process





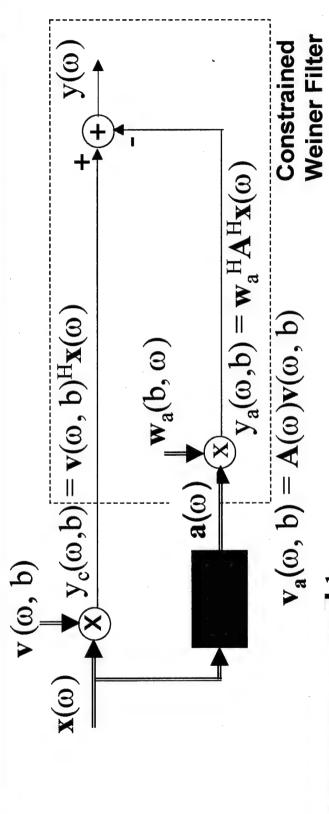
Suppress @ and b:

$$\mathbf{w}_{a} = \mathbf{R}_{aa}^{-1} \left(\mathbf{r}_{ac}^{H} - \left(\frac{\mathbf{r}_{ac}^{H} \mathbf{R}_{aa}^{-1} \mathbf{v}}{\mathbf{v}_{a}^{H} \mathbf{R}_{aa}^{-1} \mathbf{v}} \right) \mathbf{v}_{a} \right)$$



Steering Invariant DR Sidelobe Cancellation (SISC) Process





Suppress @ and b:

$$= \frac{\mathbf{v} - \mathbf{A} \mathbf{w}_a}{1 - \mathbf{w}_a^H \mathbf{A}^H \mathbf{v}}$$

$$\mathbf{w}_{a} = \mathbf{R}_{aa}^{-1} (\mathbf{r}_{ac} - \alpha \mathbf{v}_{a})$$



Robustness Management Robust Robustness (RR):



CBF (v) and unconstrained ABF (w₀) linear blend

$$\mathbf{w} = (1 - \beta) \mathbf{v} + \beta \mathbf{w}_0,$$

where on a beam-by-beam as-needed basis (RR),

$$\beta = \begin{cases} 1, \text{ for } |\mathbf{w}_0 - \mathbf{v}|^2 \le G \\ \frac{G^{1/2}}{\left||\mathbf{w}_0 - \mathbf{v}||^2 + G\right|} \end{cases}$$

$$G = WNGC - 1$$
.

For a Sidelobe Cancellation ABF

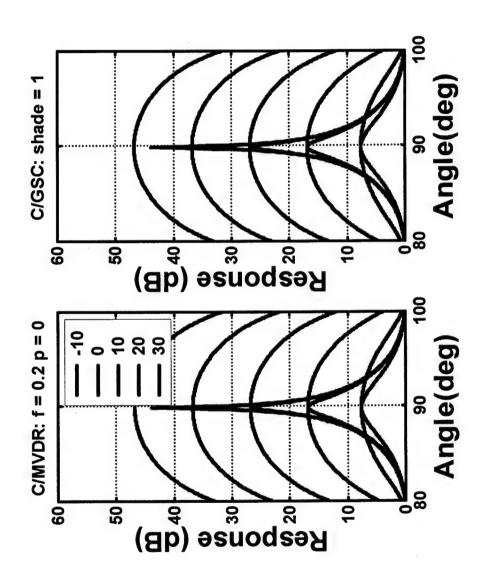
$$\mathbf{w}_0 = \mathbf{v} - \mathbf{A}\mathbf{w}_a$$

and the

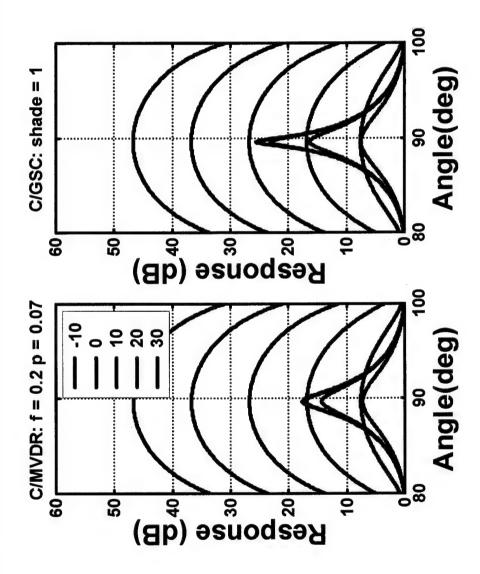
$$\mathbf{w} = \mathbf{v} - \beta \mathbf{A} \mathbf{w}_a$$
 (really simple!).



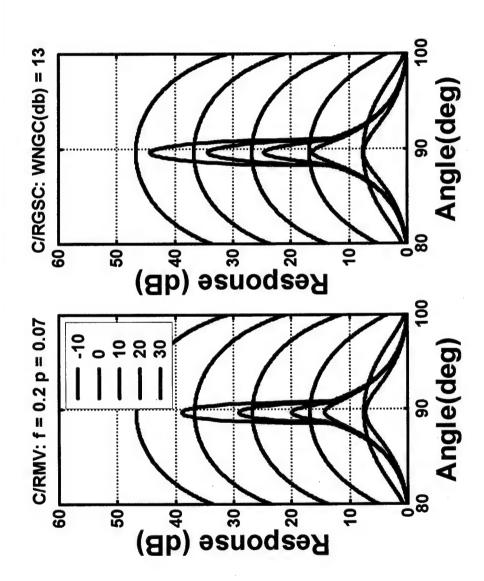




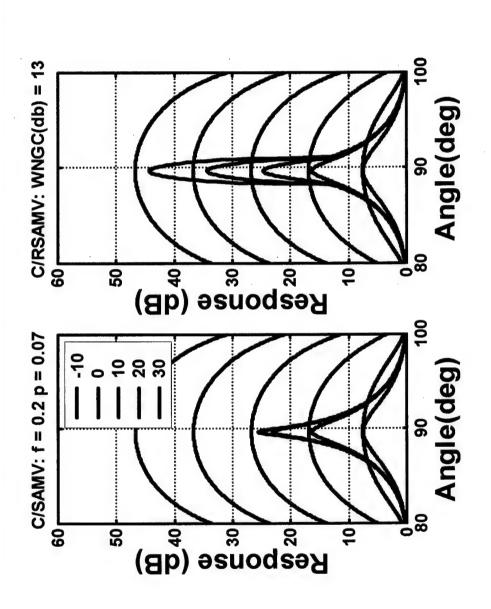








Subarray Preprocessing w/o (I) and with (r) RR; NumHydPerSA = 6 (M = 8, N = 48, pert=0.07)

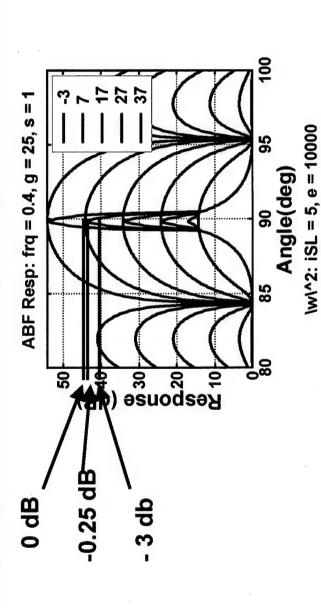




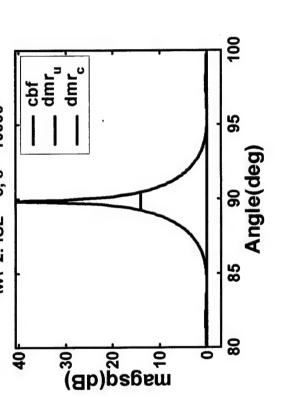
Blended CBF-DMR Point Design

(Owsley, SAM 02)





Design Procedure:
One step pre-solution
for G in terms of
specified allowable
signal suppression v.



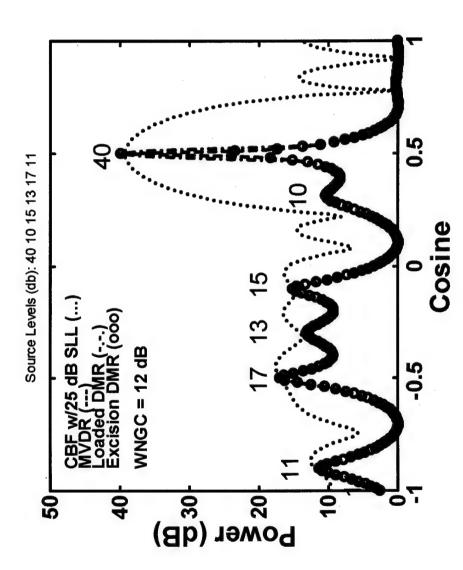




Six Stationary Sources: ES

(pert = 0.0, N = 48, D = 7, f = 0.2, sa group size = 4)

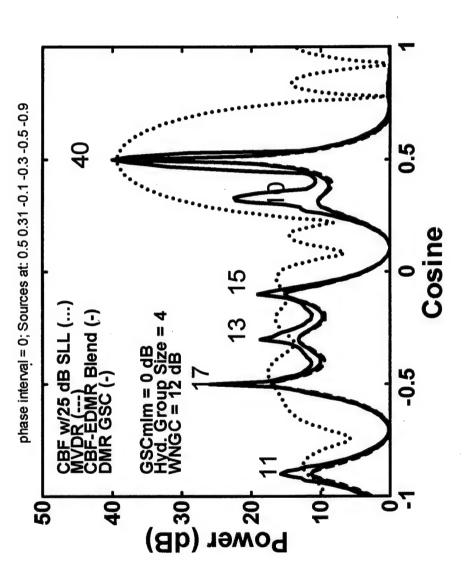






Six Stationary Sources

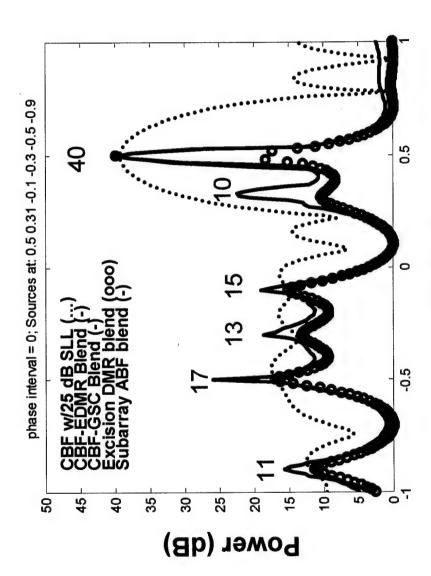
(pert = 0.0, N = 48, D = 7, f =0.2, sa group size = 4)





(pert = 0.0, N = 48, D = 7, f =0.2, sa group size = 4)





Cosine

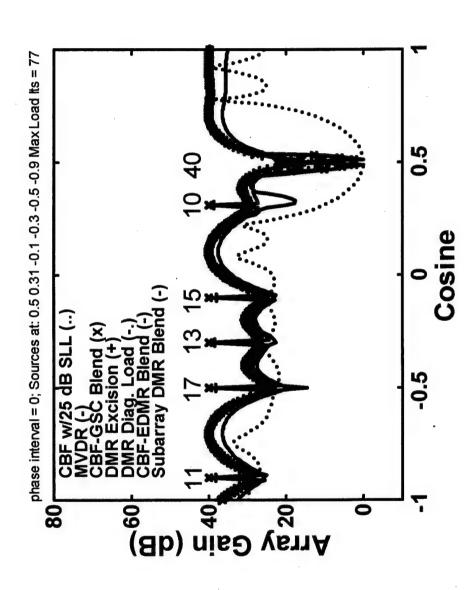




Six Stationary Sources

(pert = 0.0, N = 48, D = 7, f = 0.2, sa group size = 4)

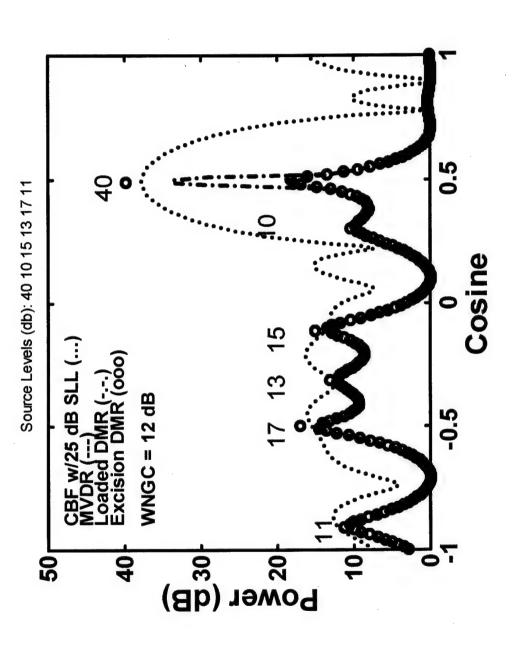








Six Stationary Sources (pert=0.07, D = 7, N=48, M=12, f =0.2, sa group size = 4)





Six Stationary Sources (pert=0.07, D = 7, N=48, M=12, f =0.2, sa group size = 4)



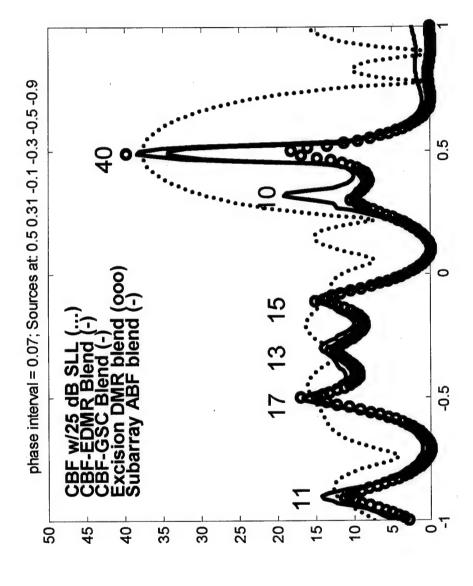


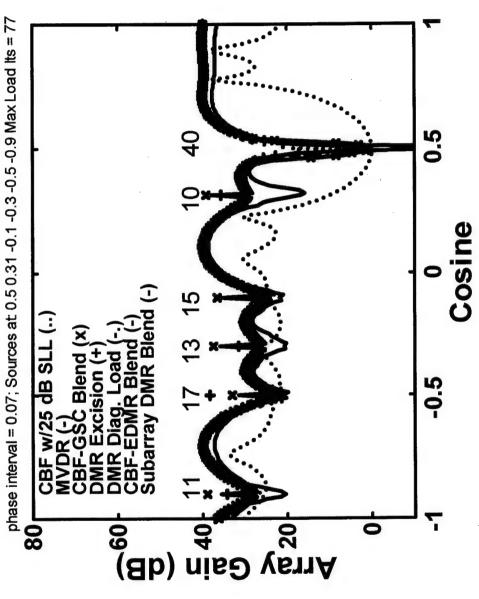
Figure 5.3







phase interval = 0.07; Sources at 0.5 0.31 -0.1 -0.3 -0.5 -0.9 Max Load Its = 77



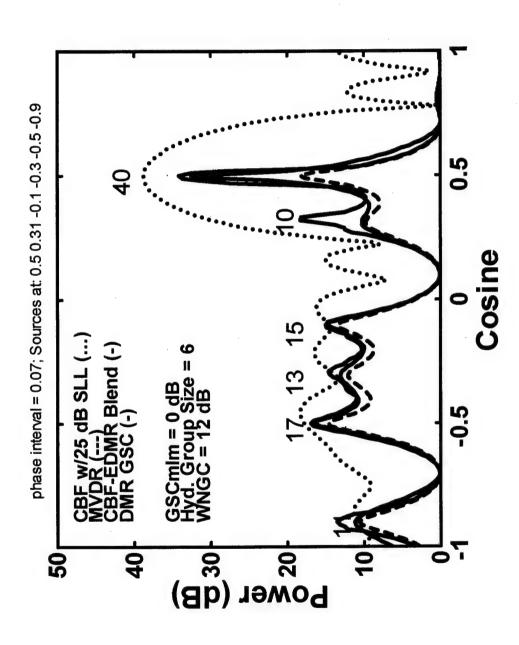




Six Stationary Sources

pert =0.07, N =48, M = 8, D = 7, f =0.2, number of sensors per sa = 6)



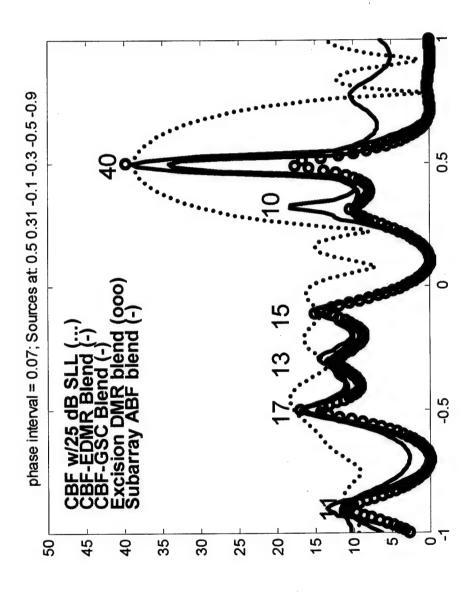








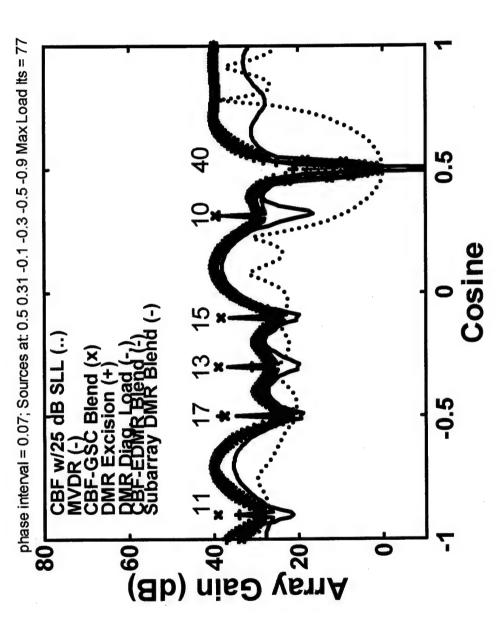






Six Stationary Sources (pert =0.07, N =48, M = 8, D = 7, f =0.2, number of sensors per sa = 6)

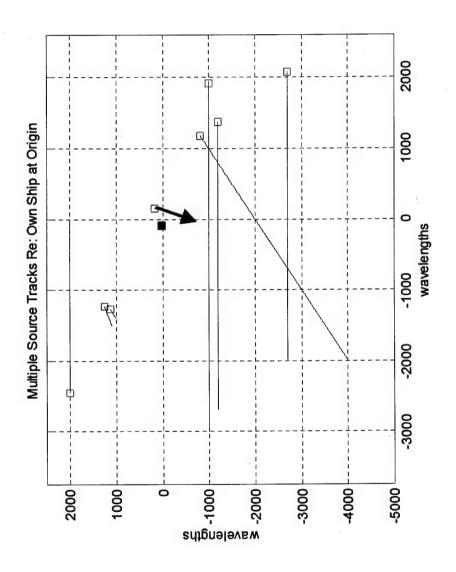






Ship Tracks: 30 Minute Event

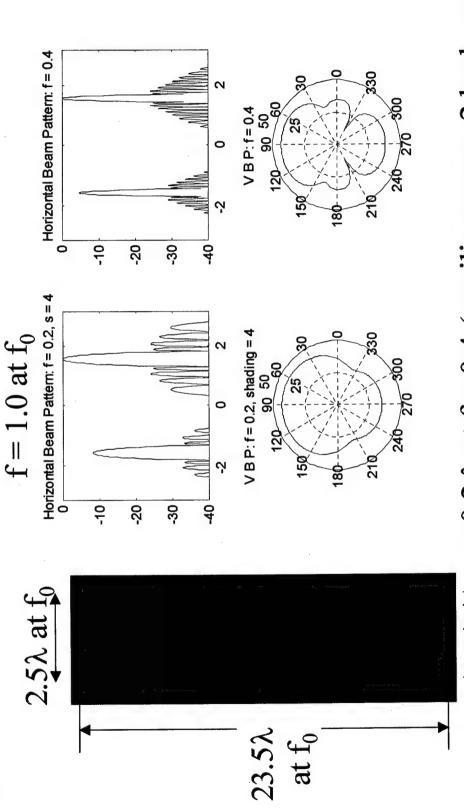




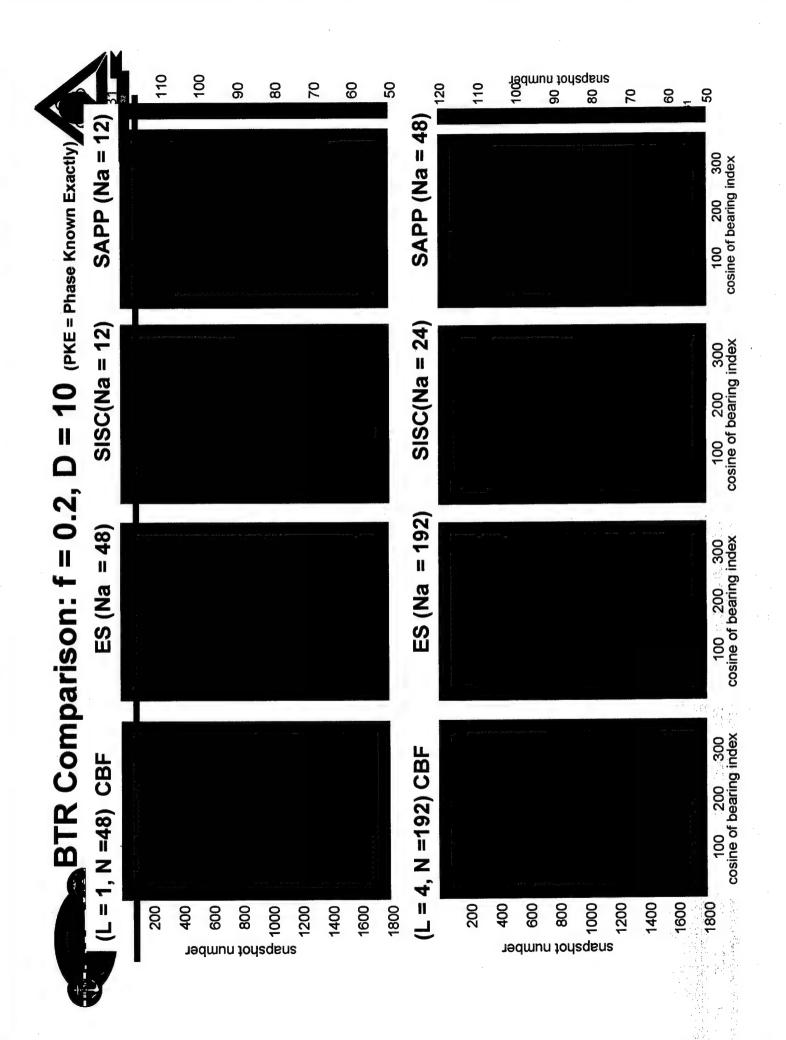


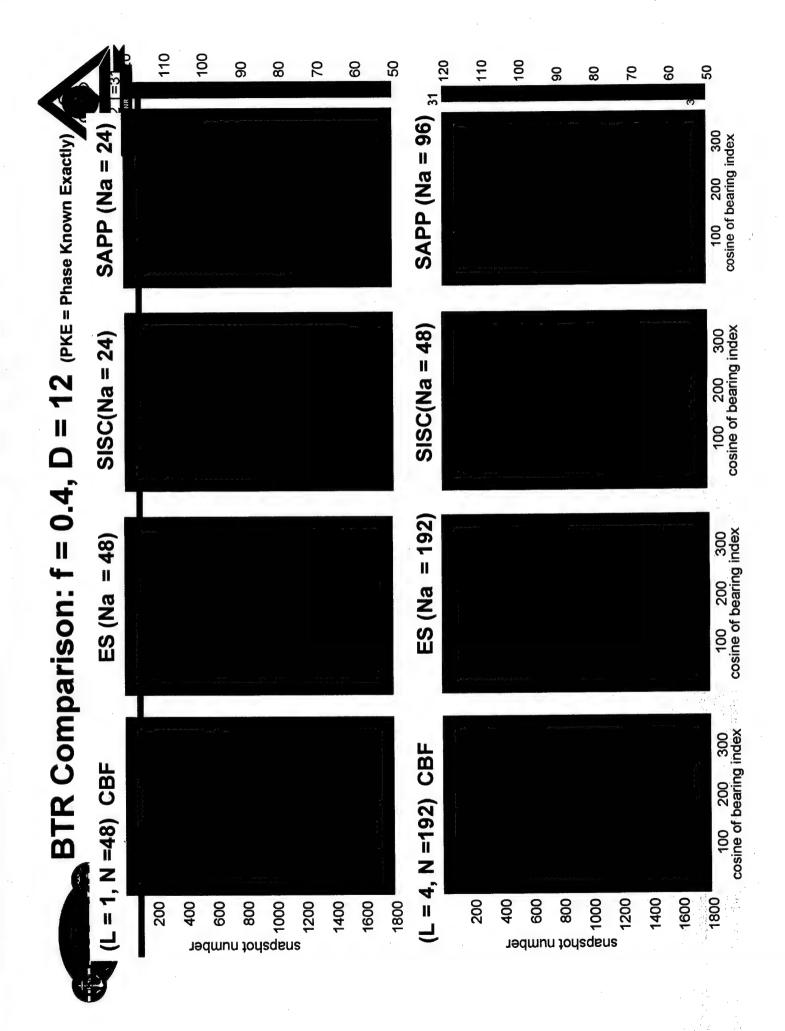
ONR Acoustic Observatory Segment (L = 1, N = 48) or (L = 4, N = 192)





-0.2 λ at f = 0.4 (auxiliary array 2 hyd. groups) 0.25λ at f = 0.2 (auxiliary array 4 hyd. groups)

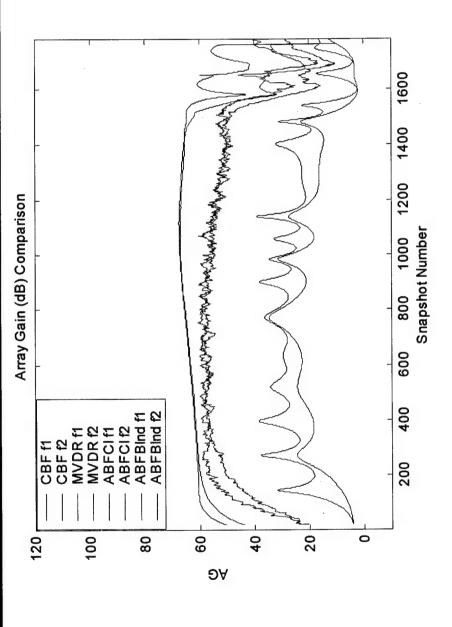






AG ES DMR: N = 48, D = 10/12

(PKE WNGC = 12 db)

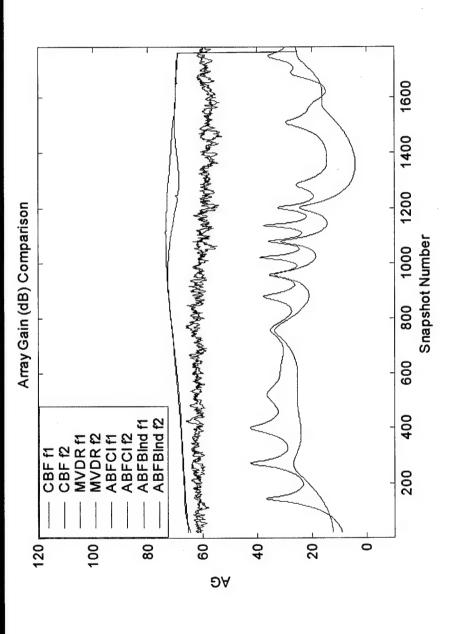






AG ES DMR: N = 192, D = 10/12

(PKE WNGC = 12 db)



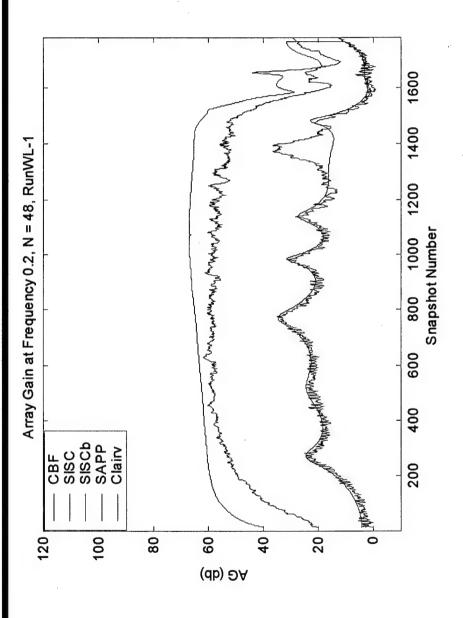




AG DMR: f = 0.2, N_a = 12, D = 10

(PKE)

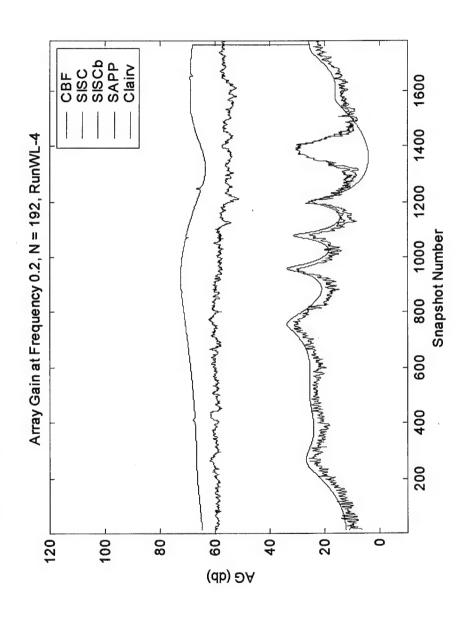






AG SA/SC DMR: f = 0.2, N = 192, D = 10/12

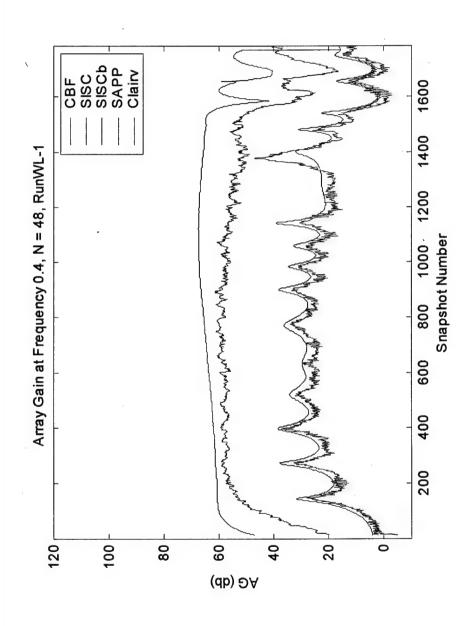






AG DMR: f = 0.4, $N_a = 24$, D = 12

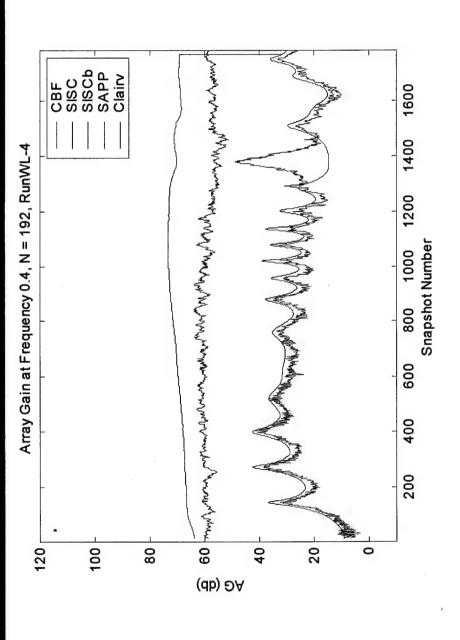






AG SA/SC DMR: f = 0.4, N = 192, D = 10/12

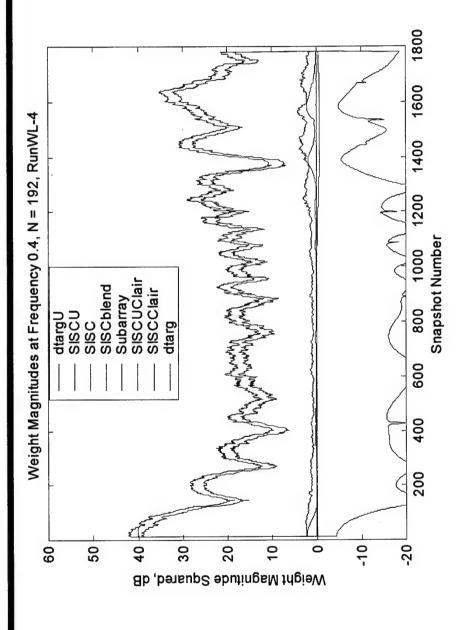






Stochastic v. Clairvoyant Weight Vector MS Clue to SISC AG Degradation:







Final Comments



Beam, subarray, auxiliary (sparseness is key) Candidate ABF spaces for efficient DMR ABF:

Adaptation space sample vector should/can be independent of beam steering direction and have N_a order O(D + safety factor).

The Steering Invariant Sidelobe Canceller (SISC) is an auxiliary space method that can "hedge" on the spatial sampling theorem and increase efficiency. AG is an open issue.

"Measure" the need for ABF at higher frequencies.

without an infinite number of beams suppresses loud sources Signal Suppression v. Spatial Resolution: Clairvoyant ABF but, by definition, produces "the best" spatial resolution.



BACKUP

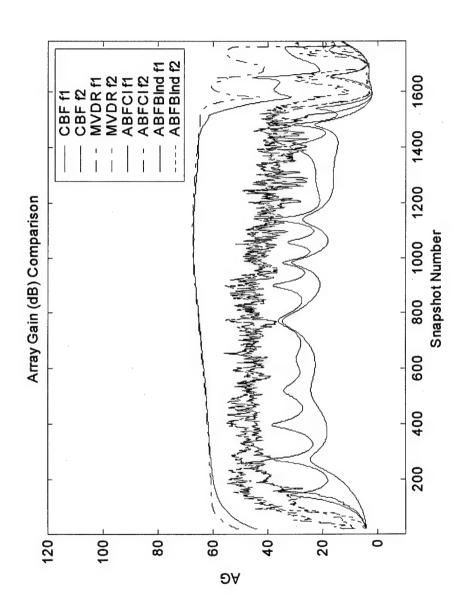






AG ES DMR: N = 48, D = 10/12 (2 degree phase pert)







Session V: Sonar I (Classified)



Adaptive Beamforming with the T-16 Array for Broadband Detection

H. Cox/ Orincon Corporation

S. Kogon/ MIT Lincoln Laboratory

H. Lai/ Orincon Corporation

T. Phipps/ UT ARL

Adaptive Array Processing for the MK-48 Torpedo in a Shallow Water Countermeasure Scenario

A. Mirkin/ NUWC

N. Pulsone/ MIT Lincoln Laboratory

An Adaptive Beamformer for Spectrum Analysis in Passive Sonar Systems

S. Kogon/ MIT Lincoln Laboratory

K. Arsenault/ MIT Lincoln Laboratory

Sub-Aperture Beamspace Adaptive Array Processing

H. Freese/ SAIC

B. Sperry / SAIC

K. Votaw//SAIC



Session V: Sonar I - Themes



Detection v. Classification in Clutter

ABF for Detection in Clutter

- Spatial resolution is key
- Aggressive/minimally constrained BB ABF
- High SNR signal suppression is acceptable

ABF for Classification in Clutter

- Minimum spectral distortion is key
- Highly constrained mainlobe ABF
- Must balance rejection of undesired interference in the beam with suppression of desired signal in the same beam

Rapid Adaptivity

 Reverberation, shipping dynamics, array motion and high data dimensionality



Shipping Parameters

Number of sources = 8

Source SoA = 1.5 knts.

Source SoA = 4.1 knts.

Source SoA = 8.2 knts.

Source SoA = 6.8 knts.

Source SoA = 7.5 knts.

Source SoA = 6.8 knts.

Source SoA = 0.5 knts.

Source SoA = 0.3 knts.

source Lev	Source Level Kange(w	VI) Prop Loss	Amb Leve	J SINK	SOA(WIS)	MI) Prop Loss Amb Level SNR SOA(WI/S) heading (Sourceinio - 1.0e+003)
0.1000 0.7018	0.7018	0.0569	0.0600	-0.0169	0.0600 -0.0169 0.0015 0.0800	0.0800
0.1650	2.0000	0.0660	0.0600	0.0390	0.0600 0.0390 0.0041 0.1800	0.1800
0.1700	3 1623	00200	0.0600	0.0600 0.0400 0.0082	0.0082	0

0	0.0300	0.0450
0.0068	0.0005	0.0003
0.0306	-0.0054	0.0003
0.0600	0.0600	0.0600
0.0694	0.0654	0.0647
2.9547	1.8601	1.7205
0.1600	0.1200	0.1250

0.0075

0.0320

0.0600

0.0730

4.4721

0.1650

0.0068

0.0195

0.0600

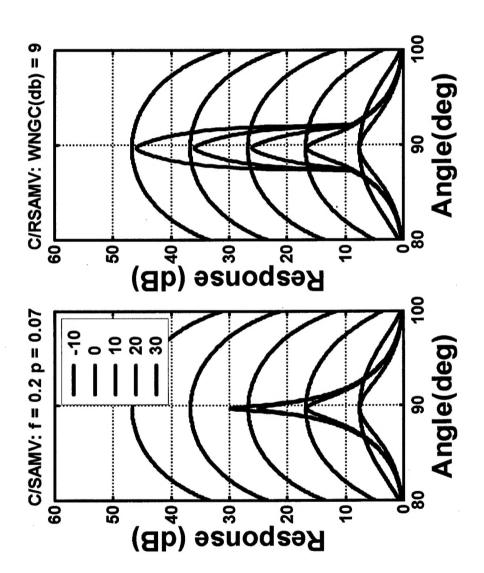
0.0705

3.3601

0.1500



Figure 3.4







Six Stationary Sources

(pert=0.07, D = 7, N=48, M=12, f =0.2, sa group size = 4)

